

A theoretical Approach Project Management & Planning of Modern Residential Building by using ETABS

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ABSTRACT

For analyzing a multi storied building one has to consider all the possible loadings and see that the structure is safe against all possible loading conditions. There are several methods for analysis of different frames like cantilever method, portal method, Matrix method. The present project deals with the analysis of a multi storied residential building of G+5 consisting of 4 apartments in each floor. The dead load & live loads are applied and the design for beams, columns, footing is obtained.

Keywords- Planning, Structural Design, ETABS,

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I. INTRODUCTION

The process of planning, designing and construction of a structure is considered to be providing modern facilities & comfortable apartment on very low budget. Our country is experiencing unprecedented Problems of urban population. There is a growing tendency of rural influx into big cities due to the developing economy and industrialization besides the growth of population. This lead to large scale construction and planning to meet the growing demand of urban population also cost of land is forcing planners to get in for "APARTMENT" and these buildings become inevitable.

1.2 STAGES IN STRUCTURAL DESIGN

There are five stages for the design of structures:

- Planning of Structure
- Drawing Study
- Load Combinations
- Analysis of Structures
- Structural Design

II. LITERATURE REVIEW

High Rise Buildings and How They Affect Countries Progression (Dr. Akram Farouk) stated that Facades must be distinct and able to achieve a good balance between form and economic cost, Creating laws and principles governing high rise buildings construction in order to stimulate capital and investment in such projects formation of various an investment committee which will provide all the required economic studies in order to ensure the success of the projects.

They used ETABS for the analysis and design of a G+5 multi storied building. The dead loads acting on the slab were calculated manually while live load, seismic load and wind load have been entered by following respective IS Codes. The design was done using limit state of design according to IS 456:2000. They showed how efficiently and easily such a high rise building can be designed within a very short span of time.

PROBLEM IDENTIFICATION

Then it was designed manually following Limit State Method. After that ETABS is used to match the design and make structure optimize and economical by trying different dimension for same capacity. For quick cost prediction of Building, this study therefore examines the cost effectiveness in terms of amount of materials. In case of real life structure are used for working stress method because the structure are crack free.

III. METHODOLOGY

To achieve the objectives of the study that is to analyze and design residential building using ETABS and by manual method, which meets the basic requirements such as safety, durability, it has been proposed to follow the following methodology.

- *Site survey*
- *Soil investigation*
- *Structural planning*
- *Analysis and design in ETABS*
- *Verification by manual method*
- *Detailing*

SELECTION OF PLOT AND STUDY

- Availability of public utility services, especially water, electricity & sewage disposal.
- Contour of land in relation the building cost.
- Cost of land.
- Distance from places of work.
- Ease of drainage.
- Location with respect to school, collage & public buildings.
- Nature of use of adjacent area.
- Transport facilities.

PLANNING

The planning is done as per the building by laws rules and regulations. Its G+5 story apartment. 5 tower 4 rooms in each floor. The general rules are as

Total Area	10117.1 sq.m
Buildup Area	929.030 sq m Each tower
Apartment Area	148.64 sq.m
No of Tower	5 tower , G+5
Apartments	4 in each floor.
Lift	500kg
Gym	232.25 sq.m
Mini super market	371.61 sq.m
Club house	232.25 sq.m

Table.I.1. Area in Apartment

- The distance from Bilaspur airport 10km
- The distance from Bilaspur railway station 15km
- The main shopping market is 2km away
- All rooms have attached bathroom

APARTMENTS ARE DIVIDED INTO 3 DIFFRENT CATEGORIES ACCORDING TO INCOME GROUP:-

HIGH INCOME GROUP

Total plot area - 2500.00sq.ft.

Total built up area – 2400.00sq.ft

MINIMUM FLOOR AREA & HEIGHT OF ROOMS:-

ROOM	FLOOR AREA	HEIGHT (m)
<input type="checkbox"/> HALL	23.09sqm(248.6sqft)	3.3m
<input type="checkbox"/> DINING	8.78sqm(94.6sq.ft)	3.3m
<input type="checkbox"/> TOILET	3.84sqm(41.4sqft)	2.7m
<input type="checkbox"/> BED ROOM-a	12.26sqm(132sqft)	3.0m
<input type="checkbox"/> BED ROOM-b	11.24sqm(121sqft)	3.0m
<input type="checkbox"/> KITCHEN	8.78sqm(94.6sqft)	3.0m
<input type="checkbox"/> TERRACE	13.93sqm(150sqft)	-----
<input type="checkbox"/> TERRACE	8.78sqm(94.6sqft)	-----
<input type="checkbox"/> MIN. HIEGHT OF PLINTH	Built-up area	0.6m (2ft)
<input type="checkbox"/> MIN. DEPTH OF FOUNDATION	-----	1.5m(4.92ft)

<input type="checkbox"/>	DAMP PROOF COURSE	-----	0.02m TO 0.025m
<input type="checkbox"/>	WALL Thick(0.02m)	-----	-----

Table.1.2. HIG Area

SPECIFICATION:-

FLOOR FINISHES	ROOM – ONYX TILES IN ALL ROOMS TOILET – PORCELAIN TILES
STAIR	RAVERTINET TILES
KITCHEN	KITCHEN PLATFORM, GREEN MARBLE, SINK STAINLESSSTEEL
DOOR	FRONT DOOR - WOODEN ARCH,DOOR, INTERNAIL DOOR – WOODEN DOOR, OTHER DOOR – FLUSH DOOR.
WINDOW	WOOD ARECH & SLIDING ALUMINUM WINDOW
WALL	INTERNAL – POP AND PLASTIC PAINT EXTERIOR – CEMENT BASED PAINT
ELECTRICAL	MODULAR SWITCHES AND COPPERWIRE
WATER SUPLLIY	G.I. PIPELINE WITH 500ltr.INDIVIDUAL TANK

Table.1.3. HIG Specification

COST ESTIMATING

COST ESTIMATING		
Building cost Rs.2500 sq.m	152 sq.m built-up area	228000/-
Foundation	1%	228228/-
Architectural	1%	230510.28/-
Water supply	6%	244340.89/-
Electric installation	12%	273661.79/-
Fire and sound resistance	20%	328394.14/-
Other service	2.5%	336603.99/-
Supervision charge	5%	353434.18/-
	Total	

Table.1.4. HIG Cost Estimating

MEDIUM INCOME GROUP

Total plot area - 2000.00sq.ft.

Total built up area – 1800.00sq.ft.

MINIMUM FLOOR AREA & HEIGHT OF ROOMS:

Table.1.5. MIG Area

	ROOM	FLOOR AREA	HEIGHT (m)
<input type="checkbox"/>	HALL	23.09sqm(248.6sqft)	3.3m
<input type="checkbox"/>	DINING	8.78sqm(94.6sq.ft)	3.3m
<input type="checkbox"/>	TOILET	3.84sqm(41.4sqft)	2.7m
<input type="checkbox"/>	BED ROOM-a	10.21sqm(110sqft)	3.0m
<input type="checkbox"/>	BED ROOM-b	11.24sqm(121sqft)	3.0m
<input type="checkbox"/>	KITCHEN	6.74sqm(72.6sqft)	3.0m
<input type="checkbox"/>	TERRACE	12.07sqm(130sqft)	-----
<input type="checkbox"/>	TERRACE	6.74sqm(72.6sqft)	-----
<input type="checkbox"/>	MIN. HIEGHT OF PLINTH	Built-up area	0.6m (2ft)
<input type="checkbox"/>	MIN. DEPTH OF FOUNDATION	-----	1.5m(4.92ft)
<input type="checkbox"/>	DAMP PROOF COURSE	-----	0.02m TO 0.025m
<input type="checkbox"/>	WALL Thick(0.02m)	-----	-----

COST ESTIMATING

COST ESTIMATING		
Building cost Rs.2500 sq.m	152 sq.m built up area	228000/-
Foundation	1%	228228/-
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Water supply	6%	244340.89/-
Electric installation	12%	273661.79/-
Fire and sound resistance	20%	328394.14/-
Other service	2.5%	336603.99/-
Supervision charge	5%	353434.18/-
	Total	

Table.1.6. MIG

Cost Estimation

SPECIFICATION

FLOOR FINISHES	ROOM – ONYX TILES IN ALL ROOMS TOILET – PORCELAIN TILES
STAIR	RAVERTINET TILES
KITCHEN	KITCHEN PLATFORM, GREEN MARBLE, SINK STAINLESSSTEEL
DOOR	FRONT DOOR - WOODEN ARCH, DOOR, INTERNAL DOOR – WOODEN DOOR, OTHER DOOR – FLUSH DOOR.
WINDOW	WOOD ARCH & SLIDING ALUMINUM WINDOW
WALL	INTERNAL – POP AND PLASTIC PAINT EXTERIOR – CEMENT BASED PAINT
ELECTRICAL	MODULAR SWITCHES AND COPPER WIRE
WATER SUPPLY	G.I. PIPELINE WITH 500ltr. INDIVIDUAL TANK

Table.1.7. MIG Specification

LOW INCOME GROUP:-

Total plot area - 1500.00sq.ft.

Total built up area – 1450.00sq.ft.

MINIMUM FLOOR AREA & HEIGHT OF ROOM:-

	ROOM	FLOOR AREA	HEIGHT (m)
<input type="checkbox"/>	HALL	36.69sqm(395sqft)	3.3m
<input type="checkbox"/>	TOILET	3.84sqm(41.4sqft)	2.7m
<input type="checkbox"/>	BED ROOM-a	8.36sqm(90sqft)	3.0m
<input type="checkbox"/>	BED ROOM-b	9.82sqm(105.8sqft)	3.0m
<input type="checkbox"/>	KITCHEN	5.98sqm(64.4sqft)	3.0m
<input type="checkbox"/>	MIN. HEIGHT OF PLINTH	Built-up area	0.6m (2ft)
<input type="checkbox"/>	MIN. DEPTH OF FOUNDATION	-----	1.5m(4.92ft)
<input type="checkbox"/>	DAMP PROOF COURSE	-----	0.02m TO 0.025m
<input type="checkbox"/>	WALL Thick(0.02 TO 0.3m)	-----	-----

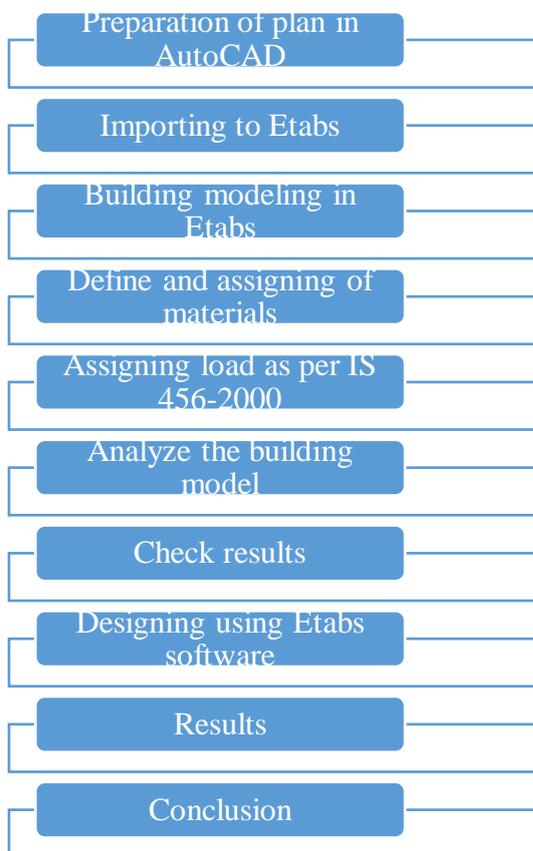
Table.1.8.LIG Area

SPECIFICATION:-

FLOOR FINISHES	ROOM- PORCELAIN TILES IN ALL ROOMS TOILET – MARBLE TILES PORCH – GRANITE TILES
STAIR	CERAMIC TILES
KITCHEN	GREEN MARBLE, SINK STAINLESS STEEL
DOOR	FRONT DOOR - WOODEN ARCH,DOOR, INTERNAIL DOOR – WOODEN DOOR, OTHER DOOR – FLUSH DOOR.
WINDOW	WOOD ARECH & SLIDING ALUMINUM WINDOW
WALL	INTERNAL – POP AND PLASTIC PAINT EXTERIOR – CEMENT BASED PAINT
ELECTRICAL	MODULAR SWITCHES AND COPPERWIRE
WATER SUPLLIY	G.I. PIPELINE WITH 500ltr.INDIVIDUAL TANK

Table.1.9. LIG Specification

MODELING AND DESIGN



Layout Plan

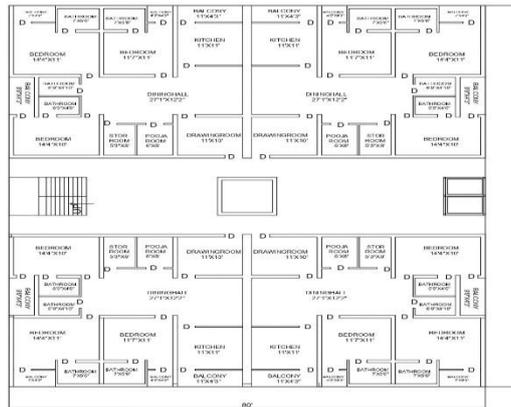


Fig 4.2.1. Layout Plan

Column Position

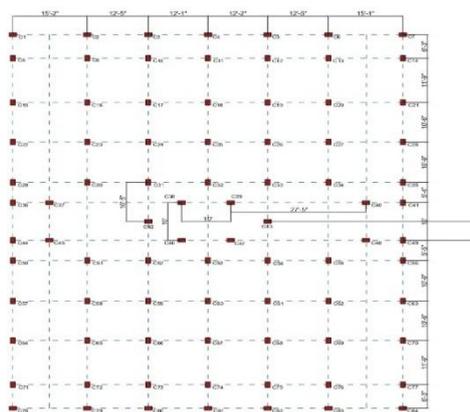


Fig 4.2.2. Column Position

PROPERTIES

This chapter provides property information for materials, frame sections, shell sections, and links.
 Frame Section

Name	Material	Shape
Column300x450	M35	Concrete Rectangular
Column 450x350	M35	Concrete Rectangular
Beam300x450	M35	Concrete Rectangular

Shell Sections

Name	Design Type	Element Type	Material	Total Thickness mm

Shear wall	Wall	Shell- Thin	M35	228.6
Slab 150 mm	Slab	Shell- Thin	M35	150
Slab 200 mm	Slab	Shell- Thin	M35	150

Table.4.3.3. Shell Sections Reinforcement Size

Name	Diameter mm	Area mm ²
12	12	113.09
16	16	201
20	20	314

Table.4.3.4. Reinforcing Bar Sizes

ANALYSIS IN ETABS AND MANUAL METHOD

The scope of the study encompasses various aspects in the structural analysis & design of building using ETABS nowadays most of the civil engineering projects are done using this software having done this project it enabled as to gain exposure in various computer applications related to civil engineering.

NAME	WEIGHT
BEAM	3.63KN/M2
COLUMN	3.63KN/M2
LIVE	2.25KN/M2
SEISMIC	1KN
WIND	39M/SEC

Table.4.4. Load type and weight

DESIGN OF SLAB

Slabs are to be designed under limit state method by reference of IS 456:2000.

When the slab are supported in two way direction it acts as two way supported slab. A two way slab is economical compared to one way slab.

SLAB DESIGN:

$f_{ck} = 20 \text{ N/mm}$ $f_y = 500 \text{ N/m}$

SPAN:

1. Shorter Span $L_x = 24.63 \text{ m}$
2. Longer Span $L_y = 30.73 \text{ m}$
3. Check $L_y/L_x = 30.73/24.63 = 1.24 < 2$

Hence Slab is Two way slab

Providing over all depth of slab is 150mm

Using 12 mm \varnothing bars and providing 15 mm clear cover

$$\text{Effective depth} = D - 15 - \varnothing/2$$

$$= 150 - 15 - 12/2 = 129 \text{ mm}$$

LOAD CALCULATION OF SLAB:

1. Dead Load = $25 \times 0.15 \times 1 = 3.75 \text{ kn/m}^2$
 2. Live Load = $1 \times 5 = 5 \text{ kn/m}^2$
 3. Load due to finish = 1 kn/m^2
- Total Load = $3.75 + 5 + 1 = 9.75 \text{ kn/m}^2$

Bending Moment Calculation:

As per IS:code 456:2000

$$a_x (+) = 0.049 \quad a_x (-) = 0.065$$

$$a_y (+) = 0.035 \quad a_y (-) = 0.047$$

The negative moment at continues edge and positive moment at mid span

$$M_x = a_x Wl_x^2$$

$$M_y = a_y Wl_y^2$$

Bending moment at mid span in shorter direction

$$\begin{aligned} 1. \quad M_x (+) &= a_x Wl_x^2 \\ &= 0.049 \times 9.75 \times (24.63)^2 \\ &= 289.82 \text{kn-m.} \end{aligned}$$

Factored bending moment $BM = 1.5 \times 289.82 = 434.73 \text{ kn-m.}$

$$\begin{aligned} 2. \quad M_x (-) &= 0.065 \times 9.75 \times (24.63)^2 \\ &= 384.45 \text{ kn-m.} \end{aligned}$$

Factored bending moment $BM = 1.5 \times 384.45 = 576.68 \text{ kn-m.}$

$$\begin{aligned} 3. \quad M_y (+) &= 0.035 \times 9.75 \times (24.63)^2 \\ &= 207.01 \text{kn-m.} \end{aligned}$$

Factored bending moment $BM = 1.5 \times 207.01 = 310.52 \text{ kn-m.}$

$$\begin{aligned} 4. \quad M_y (-) &= 0.047 \times 9.75 \times (24.63)^2 \\ &= 277.99 \text{kn-m.} \end{aligned}$$

Factored bending moment $BM = 1.5 \times 277.99 = 416.98 \text{ kn-m.}$

Check depth:

$$d = \sqrt{M/Rb}$$

$$\begin{aligned} R &= 0.36 X_{umax} / d (1 - 0.42 \times X_{umax} / d) f_{ck} \\ &= 0.36 \times 0.48 (1 - 0.42 \times 0.48) 20 = 2.75 \end{aligned}$$

$$d = \sqrt{576.68 \times 10^6 / 2.75 \times 1000} = 457 \text{ mm} < d$$

i.e. required minimum permissible depth is 100 mm

Check depth:

Mid Span

$$A_{st_{xx}} = m_{x+ve} / 0.87 \times f_y \times d \times a_1$$

$$a_1 = 1 - 0.42 \times 0.48 = 0.80$$

$$A_{st_{xx}} = 289.82 \times 10^6 / 0.87 \times 500 \times 200 \times 0.80$$

$$A_{st_{xx}} = 4164 \text{mm}^2$$

$$A_{st_{min}} = 0.12 / 100 \times 1000 \times 150 = 180 \text{ mm}^2$$

So providing minimum reinforcement

$$\text{Spacing} = 113 / 180 \times 1000 = 627 \approx 600 \text{ mm}$$

From code max. Spacing is the least of 3d and 450mm

$$3d = 3 \times 150 = 450 \text{mm}$$

Provide 12mm Ø bars @ 400mm C/C

$$A_{st_{yy}} = 310.52 \times 10^6 / 0.85 \times 500 \times 150 \times 0.80$$

$$A_{st_{xx}} = 6088.62 \text{ mm}^2$$

Provide 12mm Ø bars @ 400mm C/C

At the edges

$$A_{st_{xx}} = 384.45 \times 10^6 / 0.85 \times 500 \times 150 \times 0.80$$

$$A_{st_{xx}} = 7538.23 \text{ mm}^2$$

Specing

$$= 113 / 7538.23 \times 1000 = 14.99 \approx 15 \text{ mm}$$

Provide 12mm Ø bars @ 20mm C/C

$$A_{st_{yy}} = 416.98 \times 10^6 / 0.85 \times 500 \times 150 \times 0.80$$

$$A_{st_{xx}} = 8176.07 \text{ mm}^2$$

Specing

$$= 113 / 8176.07 \times 1000 = 13.82 \approx 14 \text{ mm}$$

Provide 12mm Ø bars @mm C/C

Corner reinforcement:

$$\begin{aligned} \text{Area of corner reinforcement} &= 3/4 \times \text{max. positive reinforcement area} \\ &= 202.5 \text{ mm}^2 \\ \text{Size of corner mash} &= 0.2 \times 7\text{m} + 1.4 \text{ m} \end{aligned}$$

Check for deflection :

$$\begin{aligned} I_x / d \times m f &= 6.09 / 0.15 \times 1.6 = 25.37 < 26 \\ I_y / d \times m f &= 6 / 0.15 \times 1.6 = 25 < 26 \end{aligned}$$

Hence, safe.

DESIGN OF BEAMS

SPAN:

B1: BEAM

1. Shorter Span $L_x = 24.63 \text{ m}$
2. Beam size = $300 \times 450 \text{ mm}$
3. Height of the wall = $10\text{ft} - 3\text{m}$

LOAD CALCULATION OF BEAM:

$$\begin{aligned} 1. \text{ Wall Load} &= 0.30 \times 3 \times 19 = 17.11 \text{ kn/m}^2 \\ 2. \text{ Self Load} &= 0.30 \times 0.45 \times 25 = 3.37 \text{ kn/m}^2 \\ 3. \text{ Slab Load (w)} &= 6 \text{ kn} \\ \text{WL}_x / 3 &= (6 \times 24.63) / 3 = 49.26 \text{ kn/m} \\ \text{Total Load} &= 17.1 + 3.37 + 49.26 = 69.73 \text{ kn/m} \end{aligned}$$

DESING OF STIRRUPS: CALCULATION OF SHEAR FORCE:

$$\begin{aligned} V_a = V_b &= \text{Total Load} \times L / 2 \\ &= 69.73 \times 24.63 / 2 = 858.72 \text{ kn} \end{aligned}$$

CALCULATION OF NORMAL SHEAR :

$$\begin{aligned} T_v = V_u / B_d &= 1.5 \times 858.72 \times 10^3 / 300 \times 450 \\ &= 9.54 \text{ kn} \end{aligned}$$

CALCULATION OF PERMISSIBLE SHEAR STRESS:

$T_c = \% \text{ of tension steel}$

$$P_t = A_{st} \times 100 / B_d$$

A_{st}

$$\begin{aligned} &= A_{st} / B_d = 0.85 / f_y \\ &= 0.85 / 500 \times 300 \times 450 \\ &= 229.5 \end{aligned}$$

$$P_t = 229.5 \times 100 / 300 \times 450$$

$$= 0.22 \%$$

$$T_c = P_t$$

$$T_c = 0.22$$

$$T_c < P_t$$

$$0.022 < 0.76$$

Hence Provide Shear Reinforcement

DESIGN OF SHEAR:

$$V_s = (T_v - T_c) / b d$$

$$= (0.76 - 0.22) / 300 \times 450$$

$$\begin{aligned} \text{Calculation } V_{us} / D(\text{cm}) &= 72.90 / 37.3 \\ &= 1.95 \text{ KN/cm} \end{aligned}$$

Hence provide 8mm dia @ 20 cm c/c spacing.

CHECK FOR SPACING:

Spacing should be provided min of the following

$$(a) 0.75d = 0.75 \times 450 = 337.5 \text{ mm}$$

$$(b) A_s v f_y / 0.4b = 2 \times (9.75^2 \times P / 4) \times 250 / 0.4 \times 300$$

$$= 99.82 \text{ mm}$$

Hence provide 6 mm dia stirrup @ 15 cm c/c spacing.

SPAN:

B2: BEAM

1. Longar Span $L_y = 30.73 \text{ m}$
2. Beam size = 300X450 mm
3. Height of the wall = 10ft – 3m

LOAD CALCULATION OF BEAM:

1. Wall Load = $0.30 \times 3 \times 19 = 17.11 \text{ kn/m}^2$
 2. Self Load = $0.30 \times 0.45 \times 25 = 3.37 \text{ kn/m}^2$
 3. Slab Load (w) = 6 kn
- WLy/3 = $(6 \times 30.73) / 3 = 182.22 \text{ kn/m}$
Total Load = $17.1 + 3.37 + 182.22 = 202.69 \text{ kn/m}$

DESING OF STIRRUPS: CALCULATION OF SHEAR FORCE:

$$V_a = V_b = \text{Total Load} \times L / 2$$
$$= 202.69 \times 30.37 / 2 = 3077.84 \text{ kn}$$

CALCULATION OF NORMAL SHEAR:

$$T_v = V_u / B_d = 1.5 \times 3077.84 \times 10^3 / 300 \times 450$$
$$= 6925140 \text{ kn}$$

CALCULATION OF PERMISSIBLE SHEAR STRESS:

$T_c = \% \text{ of tension steel}$
 $P_t = A_{st} \times 100 / B_d$
 $A_{st} = A_{st} / B_d = 0.85 / f_y$
 $= 0.85 / 500 \times 300 \times 450$
 $= 229.5$
 $P_t = 229.5 \times 100 / 300 \times 450$
 $= 0.22 \%$
 $T_c = P_t$
 $T_c = 0.22$
 $T_c < P_t$
 $0.022 < 0.76$

Hence Provide Shear Reinforcement

DESIGN OF SHEAR: $V_s = (T_v - T_c) / b d$

$$= (0.76 - 0.22) / 300 \times 450$$

Calculation $V_{us} / D(\text{cm}) = 72.90 / 37.3$
 $= 1.95 \text{ KN/cm}$

Hence provide 8mm dia @ 20 cm c/c spacing.

CHECK FOR SPACING:

Spacing should be provided min of the following

- (a) $0.75d = 0.75 \times 450 = 337.5 \text{ mm}$
- (b) $A_{sv} f_y / 0.4b = 2 \times (9.75^2 \times P / 4) \times 250 / 0.4 \times 300$
 $= 99.82 \text{ mm}$

Hence provide 6 mm dia stirrup @ 15 cm c/c spacing.

DESIGN OF COLUMN

Columns are compression members.

SELF LOAD

$$= 0.30 \times 0.45 \times 3 \times 25$$
$$= 10.125 \text{ KN}$$

WALL LOAD

$$\text{.Roof Load} = (24.63 + 30.73) / 2 \times 0.115 \times 0.91 \times 19$$
$$= 55.03 \text{ KN}$$

$$\text{.Floor Load} = (24.63 + 30.73) / 2 \times 0.30 \times 3 \times 19$$
$$= 473.32 \text{ KN}$$

SELF LOAD

.Roof Load = $(24.63 + 30.73) / 2 \times 6$
= 166.08 KN

.Floor Load = $(24.63 + 30.73) / 2 \times 6$
= 166.08 KN

BEAM LOAD

.Roof Load = $(24.63 + 30.73) / 2 \times 0.30 \times 0.45 \times 25$
= 93.43 KN

.Floor Load = $(24.63 + 30.73) / 2 \times 0.30 \times 0.45 \times 25$
= 93.43 KN

Total Roof Load = $55.03 + 166.08 + 93.43 = 314.54 \text{ kn/m}$

Total Floor Load = $473.32 + 166.08 + 93.43 = 732.83 \text{ kn/m}$

Total Load on column = $10.125 + 314.54 + 732.83 = 1057.49 \text{ kn/m}$

Column Axial load:

$P_u = 1057.49 \text{ kn/m}$

Cross section = $300 \times 450 \text{ mm}$

$P_u / f_{ck} \cdot b \cdot d = 1057.49 \times 10^3 / 20 \times 300 \times 450$
= 0.39

Calculation of Eccentricity:

$e = 1/500 + b/30$

$e = 4640/500 + 300/30$

$e = 19.28$

$e \leq 20 \text{ mm}$

$M_{ue} = P_u \cdot e$

= 1057.49×0.020

= 21.14 kn-m

$\frac{M_{ue}}{f_{ck} \cdot b \cdot d^2} = \frac{21.14 \times 10^6}{20 \times 300 \times 450^2}$
= 0.01

= 21.14 kn-m

$d'/D = 0.2$

$P/f_{ck} = 0.02$

$P = 0.02 \times 20$

$P = 0.4\% \text{ minimum } 0.8$

AREA OF STEEL

$\frac{0.8Bd}{100} = \frac{0.8 \times 300 \times 450}{100}$
= 1080 mm

No. of bars for 12mm dia

= $\frac{1080}{\frac{\pi}{4} \times 12^2}$

= 10 bars

STIRRUPS SPACING

$16 \text{ dia of main reinforcement} = 16 \times 12 = 192 \text{ mm.}$

$48 \text{ dia} = 48 \times 12 = 576 \text{ mm.}$

Provide 6 mm dia. @ 192 mm c/c when main bars size is 12 mm

DESIGN OF FOOTING

1. Size of column = $300 \times 450 \text{ mm}$

2. Load = 1500 KN

3. Self-wt. of footing = 10%

4. Bearing Capacity of soil = 250 Kn/m^2

5. Total Load = 1650 KN

6. Area of footing = $1650/250 = 6.6 \text{ m}^2$

The side of the footing be in the same ratio of column

= $0.30 \times 0.45 \times 6.6$

$$= 0.135x^2 = 6.6$$

x = 6.99 m

Short side of footing
 = 0.30x6.6
 = 1.98m

Long side of footing
 = 0.45x6.6
 = 2.97m

Proved a rectangle footing is 1.98m X 2.97m

Up ward soil pressure

$$= \frac{1650}{1.98 \times 2.97}$$

$$= 280.58 \text{ kn/m}^2 = 280 \text{ kn/m}^2$$

BENDING MOMENT CALCULATION

Maximum bending moment along y- direction longer direction

$$M_{xx} = \frac{wl}{8}(B - b)^2$$

$$= \frac{280 \times 2.97}{8}(1.98 - 0.30)^2$$

$$= 36.67 \text{ KN-m}$$

Maximum bending moment along x- direction shorter direction

$$M_{yy} = \frac{wl}{8}(B - b)^2$$

$$= \frac{280 \times 1.98}{8}(2.97 - 0.45)^2$$

$$= 123.78 \text{ KN-m}$$

DEPTH OF FOOTING

Depth of footing

$M_{yy} = Md$

$$\mu_{lim} = 0.138fckbd^2$$

$$123.78 = 0.138 \times 20 \times 2.97d^2$$

$$d = 3.88 \text{ m} = 388.59\text{mm}$$

$$d = 388.59\text{mm} = 600\text{mm}$$

$dx' = dy'$

540mm = 532mm

Reinforcement in longitudinal direction

$$A_{st} = \frac{123.78 \times 10^6}{0.87 \times 450 \times 532}$$

$$= 594.30 \text{ mm}$$

Specing

$$= \frac{\text{Area of one bar}}{A_{st}} \times 1000$$

$$= \frac{\pi/4 \times 12^2}{594.30} \times 1000$$

$$= 190.30 \text{ mm} = 150\text{mm}$$

Provide 12mm bars at 150 mm c/c

Reinforcement in shorter direction

$$A_{st} = \frac{36.67 \times 10^6}{0.87 \times 300 \times 532}$$

$$= 264.09 \text{ mm} = 260 \text{ mm}$$

Specing

$$= \frac{\text{Area of one bar}}{A_{st}} \times 1000$$

$$= \frac{\pi/4 \times 12^2}{260} \times 1000$$

= 434.98 mm = 200mm
Provide 12mm bars at 200 mm c/c

Two way shear
dy = 532 mm
Perimeter of critical plan
= $300 + \frac{532}{2} + \frac{532}{2} + \left\{ 450 + \frac{532}{2} + \frac{532}{2} \right\} \times 2$
= 2796 mm
Area of shaded portion
= $2.97 + 1.98 - (0.30 + 0.53) \times (0.45 + 0.53)$
= 4.13 m²

Ks
Ks = 0.5 + β < 1
 $\beta = \frac{L_x}{L_y} = \frac{300}{450}$
β = 0.66 < 1
τc
τc = 0.25√fck
τc = 0.25√20
τc = 1.11 N/mm²
Shear force resisted by concrete
= τc x area of critical plan
= 1.11 x 300 x 532
= 177156 N
= 1771.56 KN (Vue)

Shear force causing two way shear failure
= w x area of Shaded portion
= 280 x 4.95
= 1386 KN (Vud)
= Vue > Vud

One way shear for y direction
critical plan = 2.97 m
Area of shaded plan
= 2.97 \bar{x}
= $2.97 \times \frac{1.98 - 0.30}{2} - 0.53$
τc = 0.89 N/mm²

Shear force resisted by concrete
= τc x area of critical plan
= 0.89 x 2.97 x 0.532 x 1000
= 1406.23 KN (Vue)
Shear force causing one way shear failure
= w x area of Shaded portion
= 280 x 2.97 x 0.0205
= 16.63 KN (Vud)
= Vue > Vud

One way shear for x direction
critical plan = 1.98 m
Area of shaded plan
= 1.98 \bar{x}
= $1.98 \times \frac{2.97 - 0.45}{2} - 0.53$
τc = 1.44 N/mm²

Shear force resisted by concrete x- direction

$= \tau_c \times \text{area of critical plan}$
 $= 1.44 \times 1.98 \times 0.532 \times 1000$
 $= 1516.83 \text{ KN (Vue)}$
 Shear force causing one way shear failure x- direction
 $= w \times \text{area of Shaded portion}$
 $= 280 \times 1.98 \times 0.0205$
 $= 11.088 \text{ KN (Vud)}$
 $= \text{Vue} > \text{Vud}$
 Development length

$$L_d = \frac{0.87 f_y \phi}{4 \sigma_{bd}}$$

$$= \frac{0.87 \times 415 \times 12}{4 \times 5.88}$$

$L_d = 184.20 \text{ mm}$

$L_d < L_{\text{actual}}$

Check for load transfer

$= \sqrt{\frac{A_1}{A_2}}$ note gather then 2

Actual bearing stress $= \frac{P}{bd}$

Actual bearing stress $= \frac{1650 \times 10^6}{300 \times 450}$

Actual bearing stress $= 12.22 \text{ N/mm}^2$

Permissible bearing stress

$= 0.45 f_{ck} \sqrt{\frac{A_1}{A_2}}$ note smaller then 2

$A_1 = L \times B \text{ or } [b + 4D][d + 4D]$

$A_1 = 2970 \times 1980$

$A_1 = 5880600 \text{ mm}^2 = 5880.6 \text{ m}^2$

$A_2 = 300 \times 450$

$A_2 = 135000 \text{ mm}^2 = 135 \text{ m}^2$

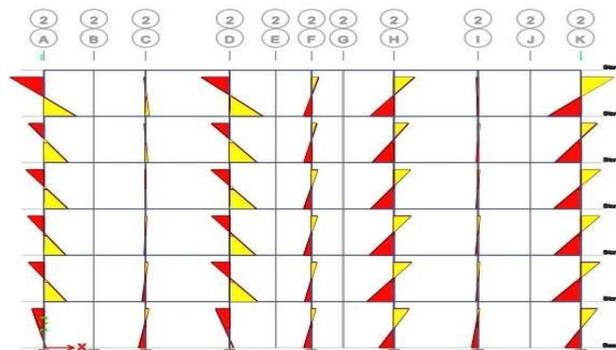
$= 0.45 \times 20 \sqrt{\frac{5880.6}{135}}$
 $= 59.4 \text{ N/mm}^2$

Actual < Permissible hence safe

IV. RESULT

Maximum Bending Moment

The below fig 5 and fig 6 tells about the maximum bending moment in 3-3 direction and shear force applied in 2-2 direction after analyzing the model.



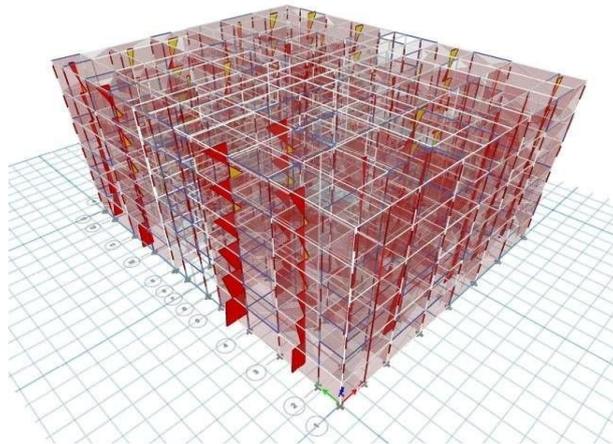


Fig 6.1.1. Maximum Bending Moment 2d & 3d

Shear Force

The below fig 5 and fig 6 tells about the shear force in 2-2 direction and maximum bending moment applied in 3-3 direction after analyzing the model.

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